

# Model Documentation of the 'Helicopter control'

## 1 Nomenclature

### 1.1 Nomenclature for Model Equations

- $x$  state vector
- $u$  control input vector
- $w$  noise vector
- $z$  regulated output vector
- $y$  measurement vector

## 2 Model Equations

State Vector and Input Vector:

$$x \in \mathbb{R}^{20} \quad u \in \mathbb{R}^4 \quad w \in \mathbb{R}^9 \quad z \in \mathbb{R}^1 \quad y \in \mathbb{R}^6$$

System Equations:

$$\dot{x}(t) = Ax(t) + B_1w(t) + Bu(t) \tag{1a}$$

$$z(t) = C_1x(t) + D_{11}w(t) + D_{12}u(t) \tag{1b}$$

$$y(t) = Cx(t) + D_{21}w(t) \tag{1c}$$

Outputs:  $z$



## 2.1 Exemplary parameter values

| Symbol         | Value         |                 |                |                |               |            |
|----------------|---------------|-----------------|----------------|----------------|---------------|------------|
| A              | 0             | 0               | 0              | 0.99857378     | 0.0533842742  | 0          |
|                | 0             | 0               | 1.0            | -0.00318221934 | 0.0595246553  | 0          |
|                | 0             | 0               | -11.5704956    | -2.54463768    | -0.0636026263 | 0.1067805  |
|                | 0             | 0               | 0.439356565    | -1.9981823     | 0             | 0.01665188 |
|                | 0             | 0               | -2.04089546    | -0.458999157   | -0.73502779   | 0.01925575 |
|                | -32.1036072   | 0               | -0.503355026   | 2.29785919     | 0             | -0.0212158 |
|                | 0.102161169   | 32.0578308      | -2.34721756    | -0.503611565   | 0.834947586   | 0.0212265  |
|                | -1.9109726    | 1.71382904      | -0.00400543213 | -0.0574111938  | 0             | 0.01398963 |
|                | 0             | 0               | 0              | 0              | 0             | -0.00593   |
|                | -5.0          | 0               | 0              | 0              | 0             | 0          |
|                | 0             | -2.0            | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0.10696        | -2.0          | 0          |
|                | 0             | 0               | -2.0           | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | -5.0           | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
| B              | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0             | 0               | 0              | 0              | 0             | 0          |
|                | 0.124335051   | 0.0827858448    | -2.75247765    | -0.0178887695  |               |            |
|                | -0.0363589227 | 0.475095272     | 0.0142907426   | 0              |               |            |
|                | 0.30449152    | 0.0149580166    | -0.496518373   | -0.206741929   |               |            |
|                | 0.287735462   | -0.544506073    | -0.0163793564  | 0              |               |            |
|                | -0.0190734863 | 0.0163674355    | -0.544536114   | 0.2348423      |               |            |
|                | -4.82063293   | -0.000381469727 | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 1.0           | 0               | 0              | 0              |               |            |
|                | 0             | 1.0             | 0              | 0              |               |            |
|                | 0             | 0               | 1.0            | 0              |               |            |
|                | 0             | 0               | 0              | 1.0            |               |            |
| 0              | 0             | 0               | 0              |                |               |            |
| 0              | 0             | 0               | 0              |                |               |            |
| B <sub>1</sub> | 0.124335051   | 0.0827858448    | -2.75247765    | -0.0178887695  |               |            |
|                | -0.0363589227 | 0.475095272     | 0.0142907426   | 0              |               |            |
|                | 0.30449152    | 0.0149580166    | -0.496518373   | -0.206741929   |               |            |
|                | 0.287735462   | -0.544506073    | -0.0163793564  | 0              |               |            |
|                | -0.0190734863 | 0.0163674355    | -0.544536114   | 0.2348423      |               |            |
|                | -4.82063293   | -0.000381469727 | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 0             | 0               | 0              | 0              |               |            |
|                | 1.0           | 0               | 0              | 0              |               |            |

### 3 Derivation and Explanation

This model is part of the "COMpleib" - library and was automatically imported into ACKREP.

The original description was:

HE7 Helicopter control "Multivariable feedback control Analysis and design"

S. Skogestad and I. Postlethwaite John Wiley and Sons, 1996, Section 12.2.4

difference  $nw=9 \rightarrow$  B1, D11, D21, rest like in HE6

### 4 Simulation

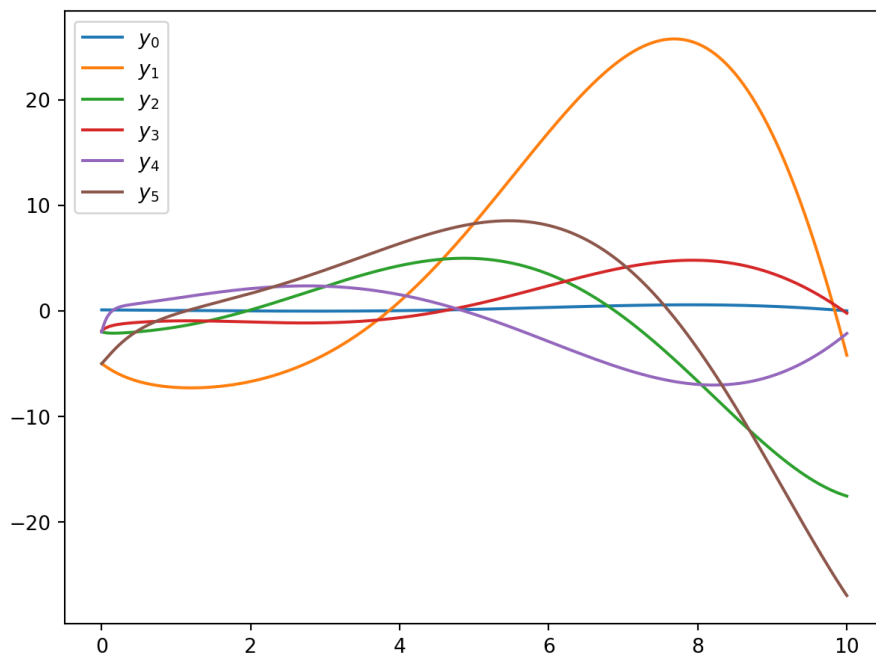


Figure 1: Simulation of the Helicopter control.

### References

- [1] "Multivariable feedback control Analysis and design" S. Skogestad and I. Postlethwaite John Wiley and Sons, 1996, Section 12.2.4 difference  $nw=9 \rightarrow$  B1, D11, D21, rest like in HE6